

厚层强非均质油藏部分射开试井曲线特征及影响因素

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摘要 针对厚层强非均质油藏部分射开井试井曲线影响因素多、解释困难的问题,基于精细数值试井方法,建立厚层强非均质部分射开试井模型,绘制典型试井曲线,总结厚层强非均质油藏的部分射开井试井曲线特征。结果表明,该试井特征曲线理论上可以分为井储段,球形流段、第一径向流段、层间窜流段和全油田平均径向流段等五段。针对厚层强非均质部分射开特征,分析了层间窜流、非均质性强弱、射开程度等参数对其试井曲线的影响规律,认为层间窜流能力主要影响了试井曲线层间窜流段出现时间的早晚;非均质强弱影响两个径向流段纵向距离;部分射开主要影响试井曲线开口大小。通过影响因素敏感性分析,降低了试井模型多解性的选择,提高了试井解释精度。利用该方法,对海外某厚层油藏进行试井解释,获得不同层的物性参数和层间窜流能力,为油藏的产能评价、射孔方案编制提供了依据。

关键词 试井; 厚层; 强非均质油藏; 窜流; 部分射开井; 试井曲线

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Characteristics of well testing curves and influencing factors for thick and strong heterogeneous reservoirs with partial perforation

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Abstract: When partially perforated, the well test curve of the thick reservoirs with strong heterogeneous has many influencing factors, which makes its interpretation very difficult. In order to solve this problem, based on the fine numerical well test method, this paper established a well test model for the thick and strong heterogeneous reservoirs with partial perforation. According to this model, a typical well test curves were drawn, and their features were summarized. The results show that, in theory, the characteristic curves of these well tests can be divided into the following five sections: well storage section, spherical flow section, first radial flow section, inter-layer channeling section and average radial flow section of the whole oilfield. According to the characteristics thick reservoirs with strong heterogeneous which was partially perforated, this paper focuses on the influence of parameters such as inter-layer channeling, heterogeneity, and the degree of perforating on the well test curve. It is found that that the inter-layer channeling mainly affects the time of occurrence of inter-layer channeling in the well test curve; the heterogeneity affects the longitudinal distance of the two radial flow sections; and the degree of perforating mainly affects the opening size of the test curve. Through the sensitivity analysis of influencing factors, the multi-solution of the well testing model is reduced, and the accuracy of well testing interpretation is improved. Using this method, the application of well test interpretation for a thick overseas reservoir was carried out. This method accurately obtains the physical parameters of different layers and the interlayer channeling capacity, which provides a basis for reservoir productivity evaluation and perforation scheme design.

Keywords: well test; thick reservoirs; strongly heterogeneous reservoir; crossflow; partial perforation well; well test curve

在实际油田开发研究过程中,常遇到厚层强非均质油藏部分射开试井解释^[1-3],由于厚油层内部的强非均质性和层间窜流引起试井曲线表现不同特征,试井解释具有多解性^[4-5]。目前,对纵向强非

均质油藏研究较少,刘能强等^[6]强调了“双层模型”的应用,并给出了试井解释的实例分析。赵春明等^[7]、张利军等^[8]给出了对于海上短时试井的一些解决方案,以降低试井多解性。魏聪等^[9]利用反褶积试井解释技术,解决了测试时间短导致的多解性问题。王志愿等^[10]、黄登峰等^[11]运用数值试井,以及联合解析试井分析方法,对复杂边界油藏及其复杂边界进行了研究和探讨。雷源等^[12]、李树松等^[13]引入数值试井技术解决了海上复杂油气田多相流和非均质等疑难试井问题。王华等^[14]、杨景海^[15]、程汉列等^[16]利用数值试井,对复杂地质模型进行研究。张俊伟^[17]对部分射开试井解释模型的应用进行了探讨,其解释成果加深了对非线性流动规律的认识,为地下渗流理论的研究和实践提供了一定参考。针对我国海相地层储层较发育、个别气藏有效厚度高达数百米、气井存在打开不完善等情況,梁海鹏等^[18]在渗流理论基础上,利用拉普拉斯变换,推导出考虑相分离影响的气井渗流数学模型和试井解释模型,提高了有水巨厚气藏试井解释精度。以上成果均是针对试井遇到的某一方面难题进行的研究。本文在以上成果的基础上,结合张利军等^[19]厚层强非均质油藏试井理论图版分析成果,针对厚层油藏中存在部分射开、纵向强非均质性、层间窜流等多个影响因素^[20-22],建立厚层强非均质部分射开数值试井模型,总结其试井曲线特征及影响因素,并对海外某实际厚层油藏进行了试井解释。

1 厚层强非均质性油藏数值试井模型

基于厚层油藏测试井的井点油层厚度、射孔厚度、测井解释的单层厚度和物性,建立厚层、强非均质性、部分射开的数值试井模型,且层间存在窜流。绘制的厚层强非均质油藏的部分射开井典型试井曲线如图 1 所示。

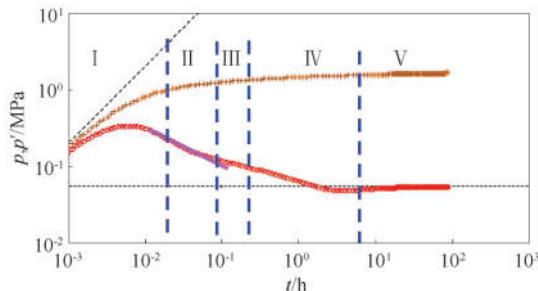


图 1 厚层强非均质部分射开井试井典型曲线

Fig.1 Typical well test curves for thick and strongly heterogeneous reservoir of partial perforation

该试井特征曲线理论上可以分为五段,即井储段、球形流段、第一径向流段、层间窜流段和全油田平均径向流段。对于该类型油藏的试井曲线特征,最大特点在于纵向强非均质性的层间窜流与双重,或者双渗油藏的层间窜流特征不一致。本模型层间窜流为双台阶状,而双重或双渗油藏的层间窜流为下凹段。

2 厚层强非均质性典型试井曲线影响因素

对于厚层、强非均质、部分射开井的试井解释,由于测试井受储层和射孔的共同影响,试井曲线表现特征较复杂,调整参数过程复杂,多解性强^[23-26]。为提高厚层部分射开试井解释精度和数值试井模型建立速度,对其试井曲线特征的影响因素及响应特征进行敏感性分析,总结不同地质参数的试井响应。

2.1 射孔层位影响分析

由于测试井部分射开,试井曲线井储后表现部分射开的特征。之后两个平行台阶,代表射开层和全井段的径向流特征,以及层间窜流。射孔层位的物性不同,其试井曲线表现特征不同。射开层物性好,第一台阶的平面流特征较明显,层间窜流台阶小,如图 2(a)所示;射开层物性差,第一台阶的平面流特征不明显,窜流发生早且现象明显,局部射开表皮系数大,如图 2(b)所示。

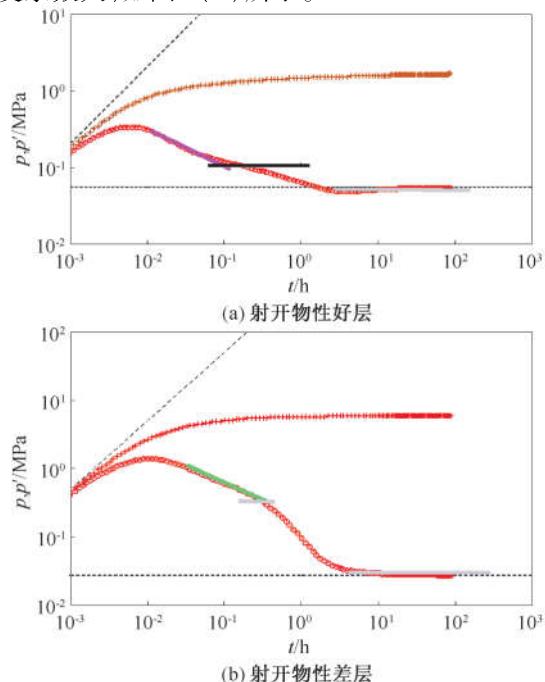


图 2 试井典型曲线图

Fig.2 Typical well test curve

2.2 渗透率影响分析

由于层厚,且纵向非均质性强,纵向不同层间的物性差异对试井响应特征影响较大。分析射开顶部层(Layer1)、未射孔其它层(Layer2、Layer3、Layer4)的不同物性对试井曲线的影响,试井设计层间物性差异见表1。

表1 不同层间渗透率试井设计方案

Table 1 Well test design scheme for permeability of different layers

方案	渗透率/(10 ⁻³ μm ²)			
	Layer1	Layer2	Layer3	Layer4
基础方案	100	10	100	10
	100	20	10	20
	100	50	20	50
	100	100	50	100
	100	500	500	500

在固定其中三层的渗透率条件下,敏感层渗透率对试井曲线影响如图3所示。

与射孔段相邻的第2层渗透率对试井曲线影响主要表现在窜流发生时间,第2层渗透率越大,窜流出现时间早,当第2层渗透率比射孔段渗透率大很多时,即级差越大局部射开表皮影响越明显。

与射孔段相邻的第3层渗透率对试井曲线影响主要表现在窜流的下凹段深度,第3层渗透率越小,凹子越明显,表现纵向整体层间差异较大。

与射孔段相邻的第4层渗透率主要影响全井段的径向流,而对窜流出现时间及窜流的下凹深度影响很小,主要是由于距离射孔段位置远,试井曲线主要表现全井段平均渗透率的特征,平均渗透率越大,越往下偏移。

2.3 射孔厚度影响分析

射孔层的不同厚度对试井曲线的影响如图4所示。射孔层厚度越小,射开不完善效应越明显,球形流特征越明显,开口越大,表皮系数越大;射孔层厚度越大,部分射开段的特征越不明显,但窜流持续的时间长,纵向强非均质性的双台阶现象明显。

2.4 层间窜流影响分析

分析与射孔层段相邻层和不相邻层间的窜流系数大小对试井曲线的影响,敏感性分析方案如图5所示。设计2套方案:方案1,分析与射孔层位相邻的层间窜流;方案2,分析与射孔层位不相邻的其它层间窜流。

窜流系数大小对试井曲线的影响如图6所示。方案1中与射孔层相连层的层间窜流越大,窜流出现时间早,而其它层间窜流对试井曲线基本不影响。

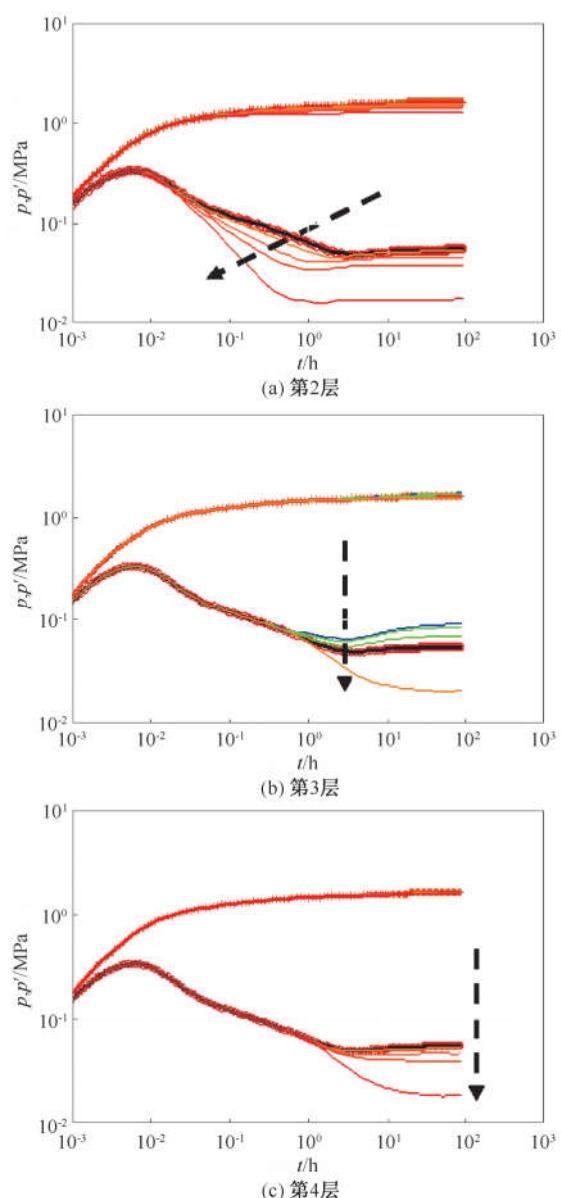


图3 不同层不同渗透率条件下试井曲线敏感性分析

Fig.3 Sensitivity analysis of well test curves for different layers with different permeability

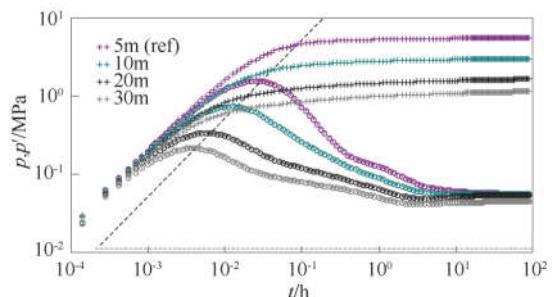


图4 射孔层不同厚度的试井曲线敏感性分析

Fig.4 Sensitivity analysis of well test curves for perforation layer with different thicknesses

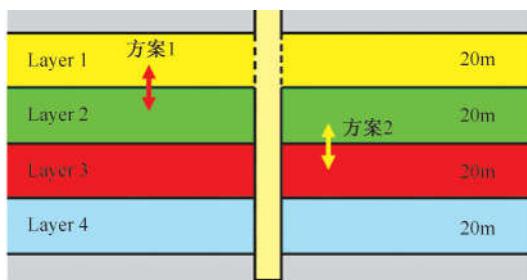


图 5 窜流系数影响的数值试井示意图

Fig.5 Schematic diagram of numerical well test affected by channeling coefficient

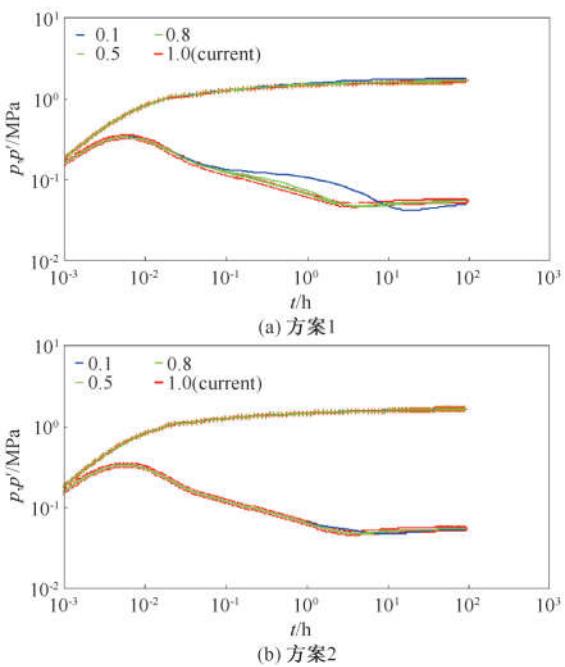


图 6 不同层间窜流系数的试井曲线敏感性分析

Fig.6 Sensitivity analysis of well test curves for channeling coefficients of different layers

2.5 水垂比敏感性分析

分析水垂比对部分射开井的试井曲线的影响,如图 7 所示。

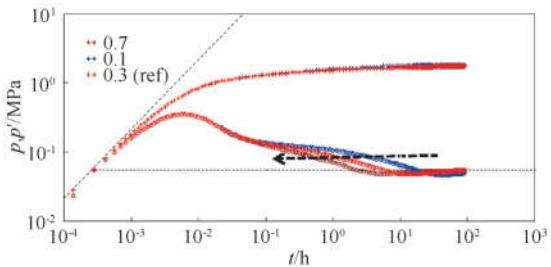


图 7 不同水垂比的试井曲线敏感性分析

Fig.7 Sensitivity analysis of well test curves with different ratios of horizontal displacement to vertical depth

水垂比主要影响窜流发生时间。该值越大,窜流出现时间早,即越容易发生层间窜流,水垂比越小,平面流的特征越明显,第一个台阶的平面径向

流持续时间也较长。

3 实例分析

海外某厚层碳酸盐岩气藏,根据岩性、地震等地质资料,纵向测井解释共 8 层,其中顶层为强风化壳,物性最好,下部层分弱风化壳,物性差,岩心和成像测井均未发现裂缝,为单孔厚层碳酸盐岩气藏。该气藏为天然能量开发,所有生产井均只射开物性好的顶部层生产。通过分析该气藏的单井生产动态以及不同深度压力监测证实,纵向上不同部位压力均有降低,表明该厚层气藏纵向连通,层间存在窜流。

测试 A 井采用井下关井测试方式测试,测试前日产气 $80 \times 10^4 \text{ m}^3$,关井 40 h,结合 A 井的测井分析成果,建立数值试井模型,如图 8 所示,纵向共 82.9 m,分 8 层,参考测井成果初始赋值不同厚度的渗透率,射孔段为顶部的 5.3 m 气层。

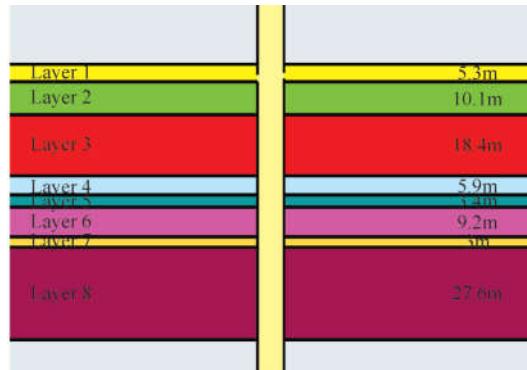


图 8 A 井数值试井示意图

Fig.8 Numerical well test diagram of well A

该井厚层部分射开的试井双对数拟合曲线如图 9 所示,出现两个径向流段。

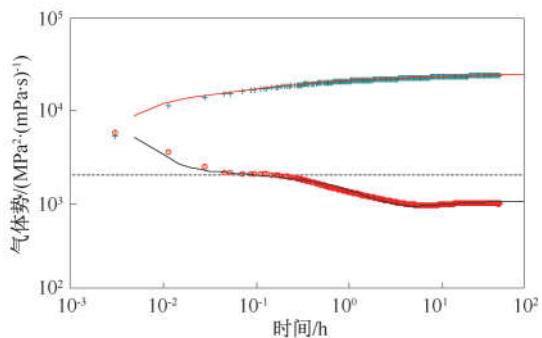


图 9 A 井试井双对数曲线拟合图

Fig.9 Double logarithmic curve fitting of well test for well A

未选择纵向多层的数值试井解释前,选择平面复合油藏解析模型进行解释,试井导数曲线完全拟合,解释复合半径 50 m,外区物性变好,与地质认识

较难达成一致;根据本文的理论模型研究和影响因素分析,建立厚层部分射开强非均质数值试井模型,调整与射开顶部层较远的底部其他层的物性,试井曲线始终很难拟合。最后选择调整射开层段和相邻2个层段的物性,以及相邻层段的层间窜流系数、水垂比参数进行试井拟合和解释。试井解释射开层物性最好,渗透率 $116 \times 10^{-3} \mu\text{m}^2$;其它层物性差,只有 $10 \times 10^{-3} \sim 30 \times 10^{-3} \mu\text{m}^2$ 左右。全井段平均渗透率为 $40 \times 10^{-3} \mu\text{m}^2$,纵向上层间存在窜流,该气藏水垂比较大,试井解释为0.7。

4 结论

(1)本文丰富了厚层、强非均质、部分射开油藏的试井理论图版,总结该试井特征曲线理论上可以分为五段,即井储段、球形流段、第一径向流段、层间窜流段和全油田的平均径向流段。

(2)通过单因素的敏感性分析,总结射孔层物性、射孔层厚度、层间窜流、水垂比等参数对厚层强非均质油藏试井曲线的影响,以及不同参数对试井曲线不同段的影响程度。该成果可以指导厚层油藏试井的快速调整参数。

(3)在厚层油藏部分射开试井解释中,不应该使用平面非均质性解释模型,而应该考虑纵向多层的强非均质性模型进行解释来降低多解性,并结合测井解释和模型拟合,给出每层物性差异和层间窜流能力,指导后期射孔方案的制定。

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